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(54) **VEHICLE BRAKE SYSTEM WITH AN ELECTRIC SERVOMOTOR AND HYDRAULIC REACTION PISTON**

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B60T 8/40 (2006.01)

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CPC **B60T 13/745** (2013.01); **B60T 8/4077** (2013.01)

(58) **Field of Classification Search**

CPC B60T 13/745; B60T 8/4077; B60T 7/042; B60T 13/04

USPC 60/553, 539, 540, 541, 545
See application file for complete search history.

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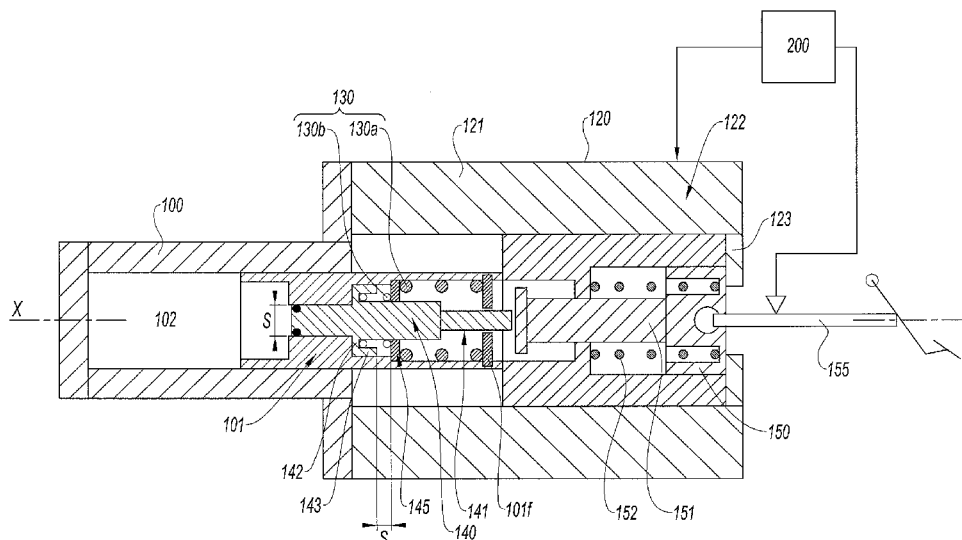
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(57) **ABSTRACT**

A brake system is described with a master cylinder actuated by a control rod connected to a plunger piston and an actuator piston acting directly on the primary piston. A hydraulic reaction piston is housed in the piston so it can be subjected to the pressure of the primary chamber and to the opposing action of a reaction spring. The plunger piston can push the reaction piston directly to push the master cylinder.

5 Claims, 7 Drawing Sheets



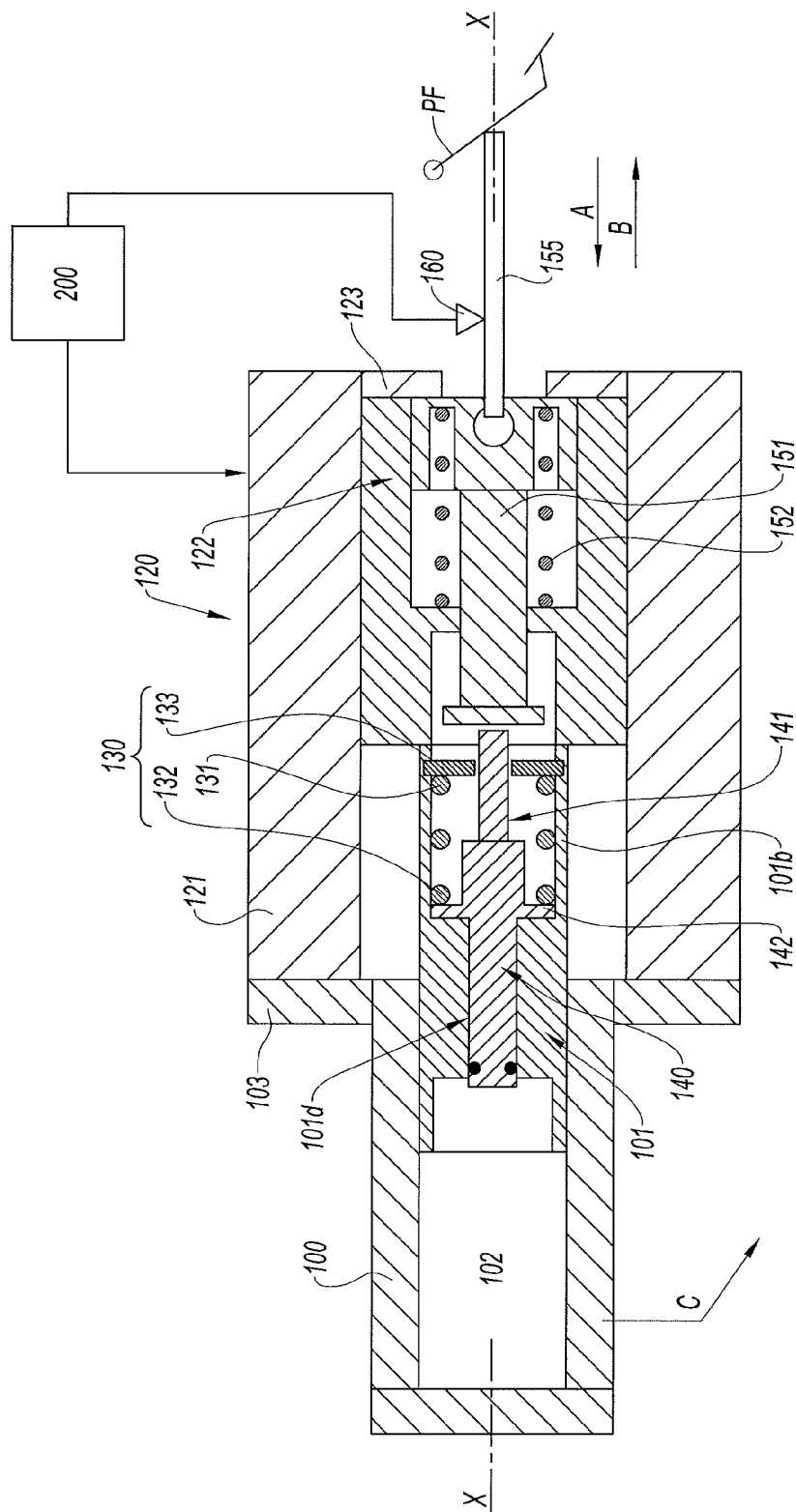


Fig. 1

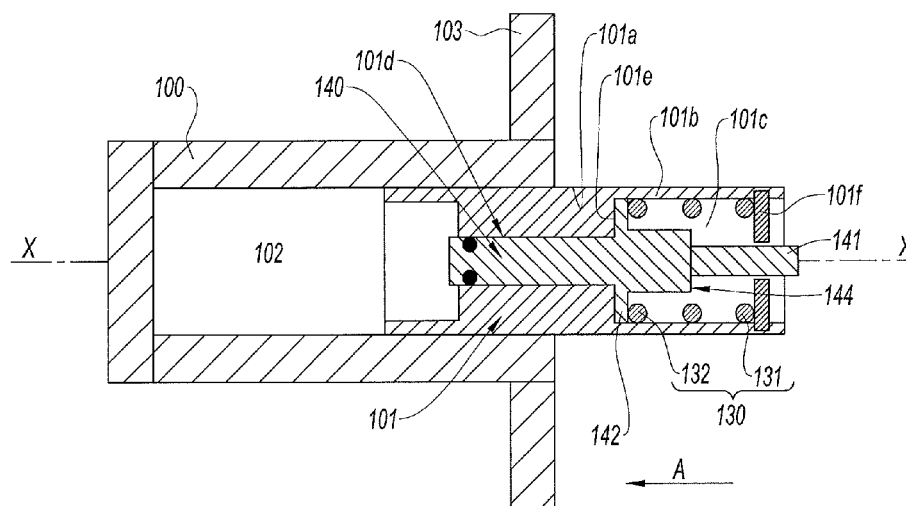


Fig. 1A

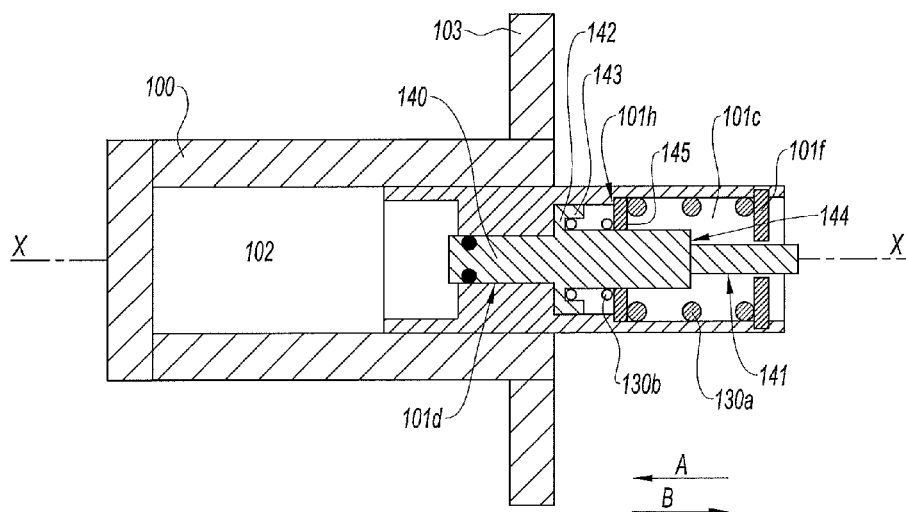
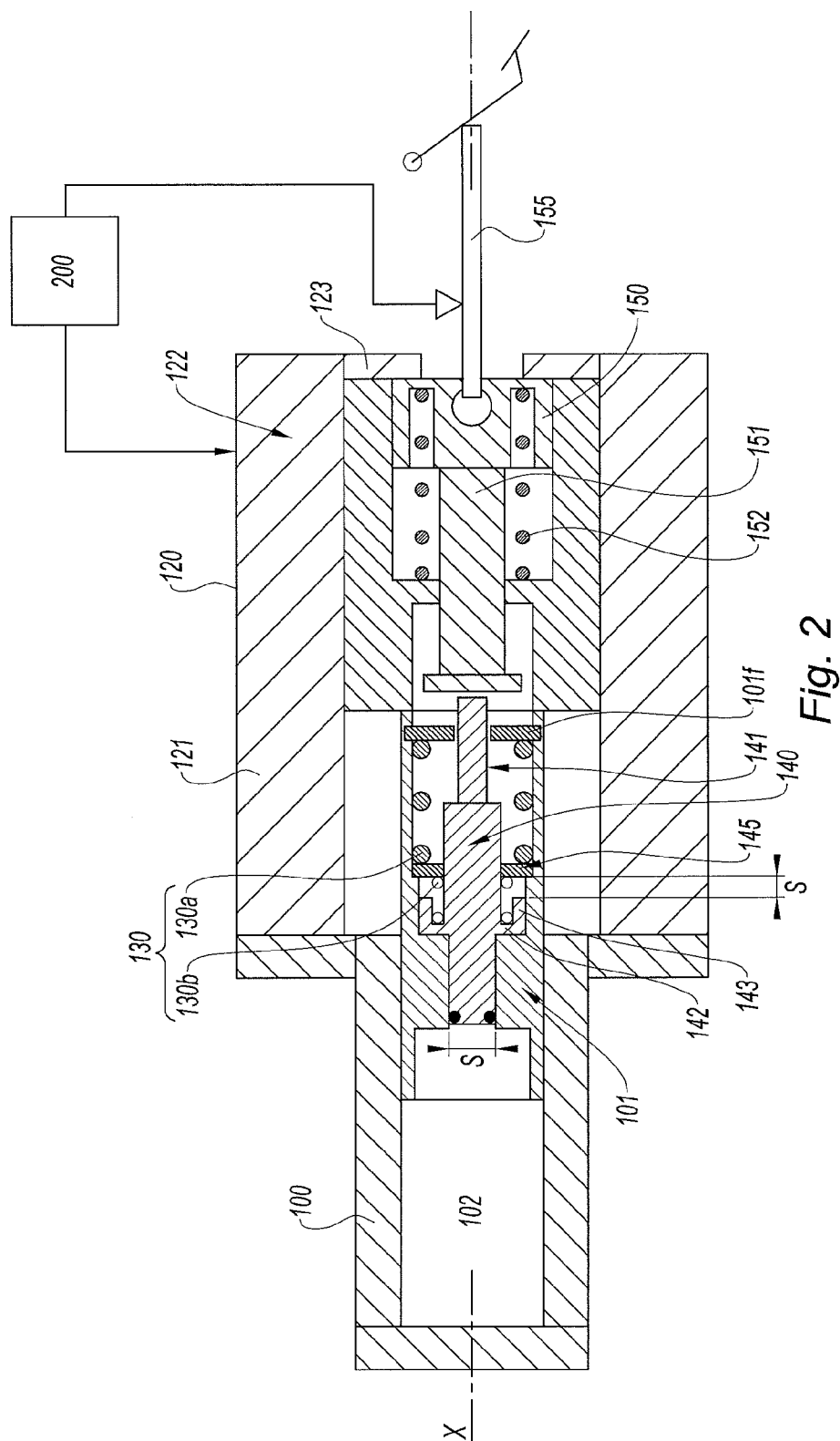


Fig. 2A



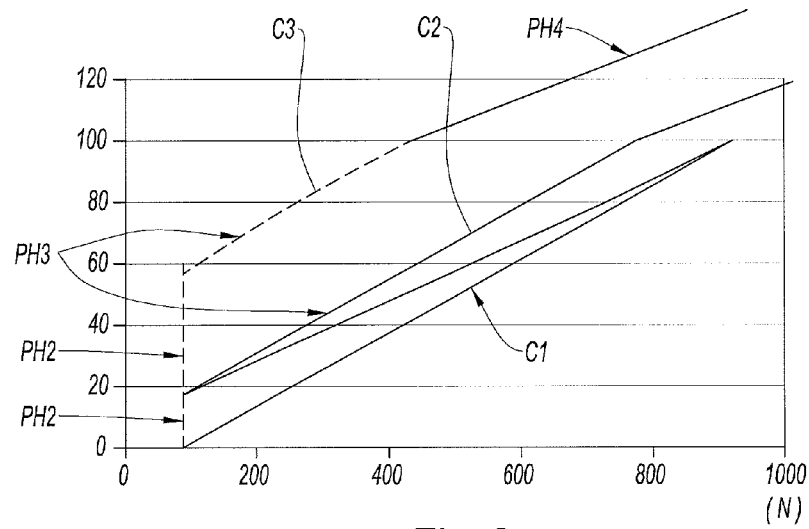


Fig. 3

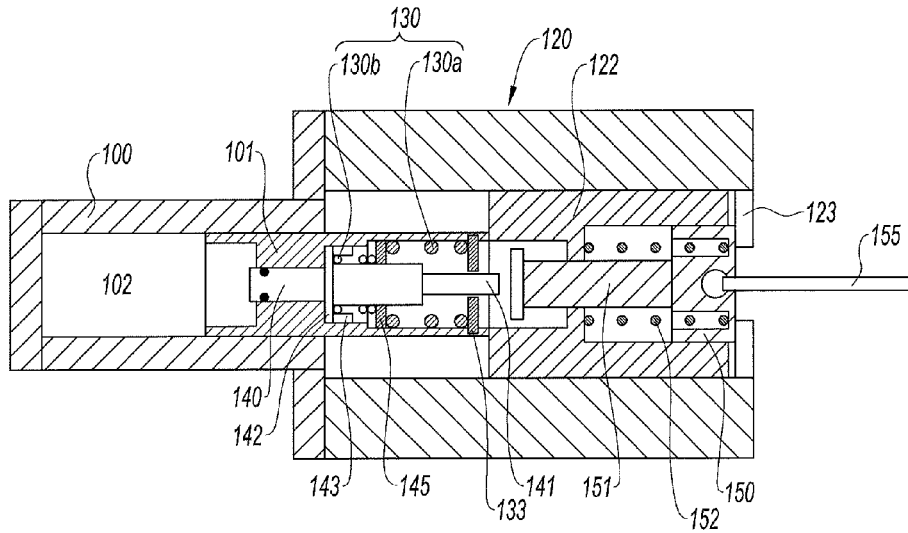


Fig. 4

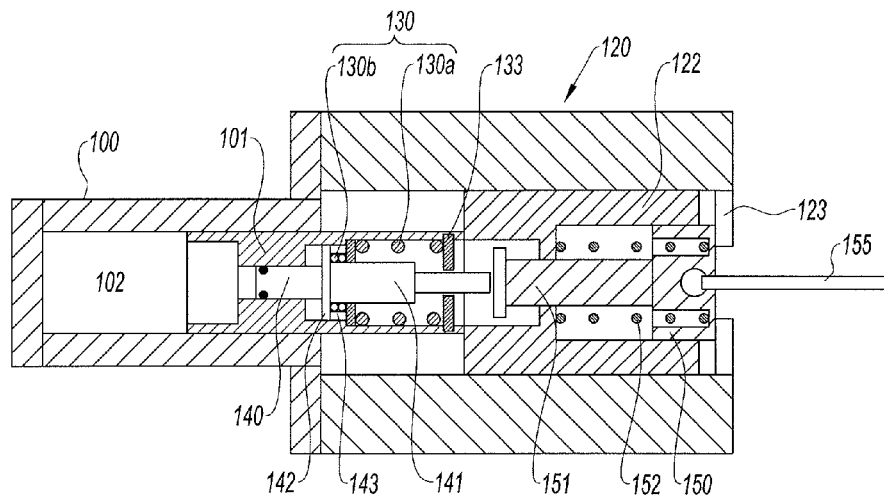


Fig. 5

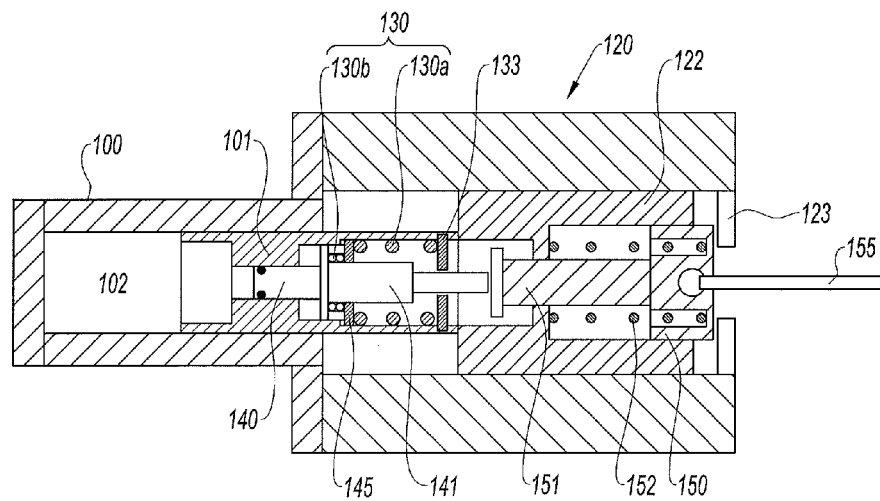


Fig. 6

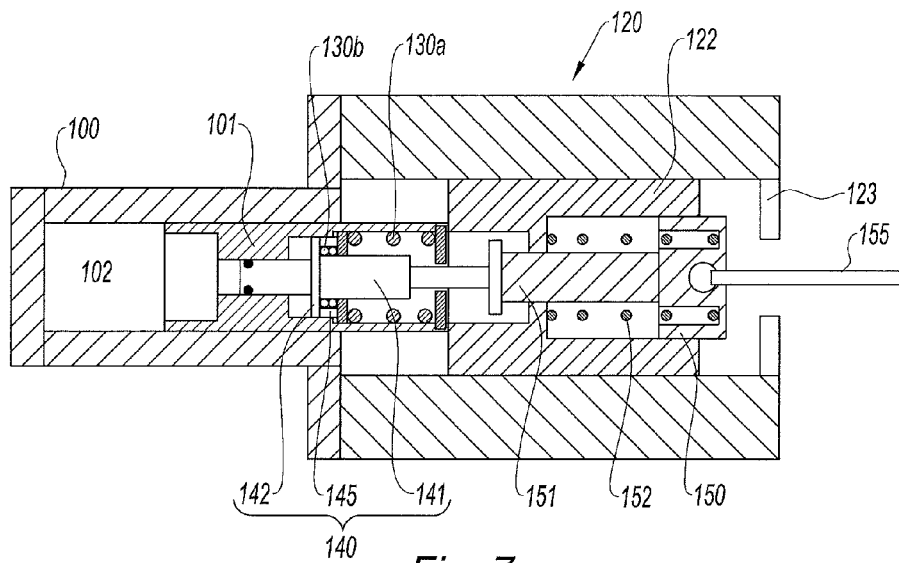


Fig. 7

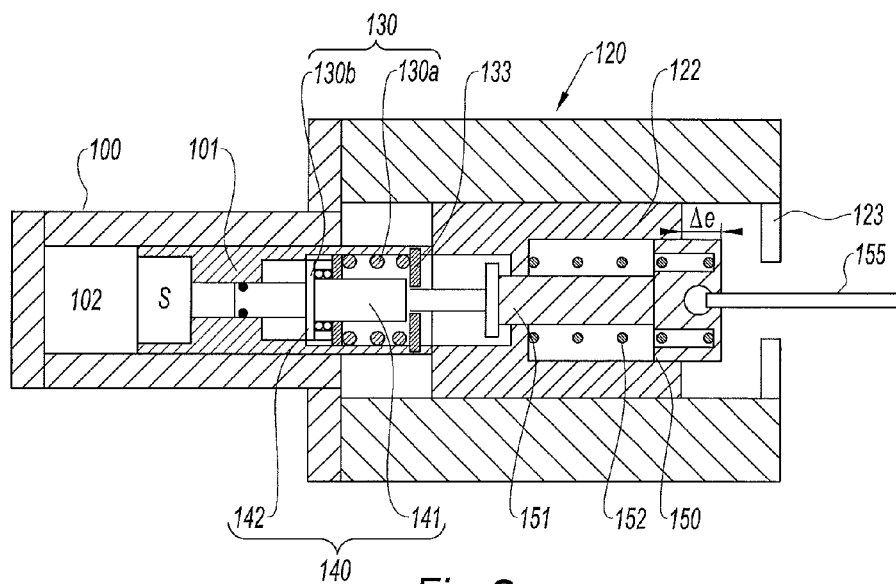


Fig. 8

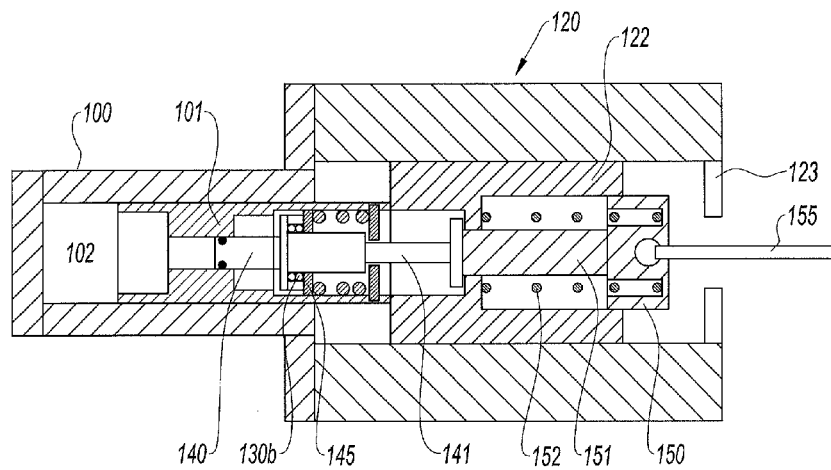


Fig. 9

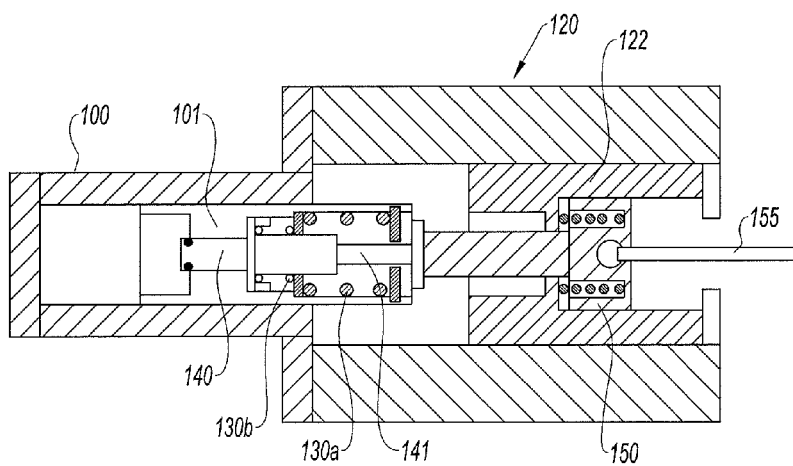


Fig. 10

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VEHICLE BRAKE SYSTEM WITH AN ELECTRIC SERVOMOTOR AND HYDRAULIC REACTION PISTON

FIELD OF THE INVENTION

The present invention relates to an electric servomotor brake system for vehicles that includes:

- a master cylinder equipped with a primary piston delimiting, in said master cylinder, a chamber connected by a brake fluid circuit to the wheel brake cylinders, and
- an electric servomotor with an actuator piston acting on the primary piston;
- a control rod connected to the brake pedal and moving a plunger piston to actuate the master cylinder, when applicable with the assistance of the electric servomotor; wherein the movement of the control rod is detected by a sensor that informs the control circuit of the electric servomotor;
- wherein the master cylinder, the servomotor, and the control rod are aligned on an axis.

BACKGROUND INFORMATION

Vehicle brake systems equipped with an electric servomotor are generally known, as in document French Patent No. 0311580, for example. Such a servomotor is equipped with a reaction disc whose sensitivity is difficult to adjust; in particular, the sensitivity of the reaction disc depends on the external temperature. Another disadvantage is the cost of the reaction disc.

An object of the present invention is a hydraulic-reaction brake system equipped with an electric servomotor that is independent of temperature, whose fabrication is less complex than known fabrications, and whose reliability and endurance is greater than one equipped with a reaction disc.

To that end, the object of the present invention is a vehicle brake system with an electric servomotor of the type described above, characterized in that

- the primary piston delimiting the primary chamber in the master cylinder is formed from a body
- that, on the exterior of the master cylinder, is extended by a cylindrical skirt forming an external chamber housing a reaction spring one end of which presses against a retaining organ integral with the skirt;
- that has an axial through hole connecting the rear of the external chamber and the primary chamber;
- the actuator piston cooperates directly with the skirt to push the primary piston;
- there is a hydraulic reaction piston;
- housed in the bore hole of the body of the primary piston; integrally bearing an axial thrust rod on the exterior;
- equipped with a stop against which the other extremity of the reaction spring rests;
- which said stop rests against the rear of the external chamber to push the primary piston or to be pushed by it.

The brake system according to the invention as described above has the advantage of especially simple fabrication and operation independent of the outside temperature with respect to pedal feel. This solution is especially reliable because it does not include a reaction disc, which is generally made of a rubbery material.

According to a particularly advantageous characteristic, the reaction spring consists of a principal spring and an auxiliary spring combined in series, separated from one another by a floating support that is mobile with respect to a primary piston stop to limit the expansion stroke of the principal

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spring, the auxiliary spring being of reduced hardness with respect to that of the principal spring so it can be compressed before the principal spring. The reaction spring is thus composed of an auxiliary spring with the interposition of a floating support to compensate for the drag of the brake against the brake disc, wherein this does not affect pedal feel.

According to another advantageous characteristic, the retaining organ is a disc traversed by the thrust rod, which is of particular interest if, according to another advantageous characteristic, the thrust rod has a shoulder that cooperates with the retaining organ to define an extreme end-of-travel position for the reaction piston.

According to another advantageous characteristic, the stop has a collar that cooperates with the floating support in compressing the auxiliary spring to limit the compression of the auxiliary spring and thereby press directly upon the floating support.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a cutaway view of a brake system composed of a master cylinder and an electric servomotor according to a first embodiment of the invention.

FIG. 1A is a partial view of FIG. 1 limited to the master cylinder and the hydraulic reaction piston.

FIG. 2 is a schematic view of a second embodiment of an electric servomotor brake system according to the invention.

FIG. 2A is a partial view of FIG. 2 limited to the master cylinder and the reaction piston.

FIG. 3 is a graph that provides the force/pressure characteristic as a function of the incoming force applied to the control rod for different brake systems.

FIGS. 4 to 10 schematically illustrate the different operating states of the brake system according to FIG. 2.

FIG. 4 illustrates a braking action at the start of the drag compensation phase.

FIG. 5 illustrates the end of the drag compensation phase.

FIG. 6 illustrates the jump transition.

FIG. 7 illustrates the application of a violent force on the brake pedal and the control rod.

FIG. 8 illustrates the application of a moderate force on the brake pedal.

FIG. 9 illustrates the implementation of braking assistance.

FIG. 10 illustrates emergency mode, with direct action of the brake pedal on the master cylinder.

DETAILED DESCRIPTION

A description of the different embodiments will be provided below for the general case of a master cylinder, **100**, combined with an electric servobrake, **120**, wherein the master cylinder can be a simple master cylinder, that is, feeding a single brake circuit, or a tandem master cylinder feeding two brake circuits. Piston **101** of this master cylinder will be referred to as primary by convention, whether it is a single piston of a simple master cylinder or the first piston (primary piston) of a tandem master cylinder. Primary piston **101** delimits, in master cylinder **100**, a chamber **102**, referred to as the primary chamber for easier identification, whether this chamber is the only chamber of the simple master cylinder or, effectively, the primary chamber of the tandem master cylinder.

According to FIGS. 1, 1A, a first embodiment of a vehicle brake system according to the invention is composed of master cylinder **100** combined with electric servomotor **120**, the assembly being aligned along axis xx, on which the various moving elements of this combination move.

Piston **101** is housed in the cylinder of master cylinder **100**, and therein delimits a primary chamber, **102**, that supplies a brake circuit, C, connected to the wheel brakes (not shown) to supply them with hydraulic fluid under pressure. Master cylinder **100** is supplied with brake fluid from a reservoir (not shown). These different, generally known, means do not require detailed explanation.

Operation of the assembly is controlled by a control circuit, **200**, that receives signals primarily for the purpose of controlling servomotor **120**.

According to FIG. 1A, primary piston **101** consists of a body, **101a**, constituting the piston properly speaking, delimiting primary chamber **102** on the interior of the master cylinder. On the exterior, body **101a** of the primary piston is extended by a skirt, **101b**, delimiting a chamber, **101c**, open to the exterior and whose rear wall, **101e**, is formed by the body of the primary piston. The body is traversed by an axial hole, **101d**, emerging in external chamber **101c** and in primary chamber **102**. External chamber **101c** houses a reaction spring, **130**, in the shape of a helical spring that approaches the interior wall of skirt **101b**. This reaction spring **130** is retained in the external chamber by stop **101f** integral with skirt **101b**, against which its extremity, **131**, rests.

Primary piston **101** houses reaction piston **140** that slides in axial hole **101d**. Reaction piston **140** is extended along the exterior by axial thrust rod **141** and has stop **142** by which reaction piston **140** can press against body **101a** of primary piston **101** or, reciprocally, by which primary piston **101** can press against reaction piston **140**. Stop **142** of the reaction piston receives the other extremity, **132**, of reaction spring **130**. Reaction spring **130**, which is a helical compression spring, thus presses stop **142** of reaction piston **140** against rear wall **101e** of the body of primary piston **101** in the absence of other forces exerted on reaction piston **140**. The thrust rod of reaction piston **140** has a shoulder, **144**, intended to limit the travel of piston **140** in direction B. Thus, reaction piston **140**, pushed in direction B, cannot be pushed beyond stop **101f**, which will encounter its shoulder **144**.

The various seals of primary piston **101** and reaction piston **140** are not shown.

According to FIG. 1, master cylinder **100** is combined with electric servomotor **120**, simply represented by its body **121**, attached to flange **103** of master cylinder **100** and constituting the stator of the motor. Servomotor **120** has actuator piston **122** controlled in a manner not shown, for example, by a ball-screw type connection, as described, for example, in document FR 0311580. The mechanical method transmitting the movement that directs actuator piston **122** does not need to be described precisely here because the only significant aspect is the fact that actuator piston **122** is controlled by servomotor **120** for its displacement from right to left (arrow A) along axis xx to act upon primary piston **101** and assist in braking.

The drive connection of actuator piston **122** is a one-way or two-way connection. In the first case, the return of actuator piston **122** at the conclusion of braking is ensured by the return forces, primarily the hydraulic forces acting on actuator piston **122**. In the second case, the return is ensured by reversing the direction of operation of the electric servomotor at the conclusion of braking.

Actuator piston **122** houses plunger piston **150**, extended in the direction of master cylinder **100** by cylindrical extension **151** and pushed by return spring **152** against rear wall **123** of housing **121** of the servomotor, which serves as a stop, just as actuator piston **122** is applied against rear wall **123** of the body of the servomotor in the neutral position of FIG. 1. Plunger piston **150** is connected to control rod **155**, itself

connected to brake pedal PF. Control rod **155** is displaced by an action on the brake pedal that pushes plunger piston **150** under conditions that will be described below.

The movement of control rod **155** or plunger piston **150** is detected by motion sensor **160**, which sends an actuator signal to control circuit **200**, which manages the operation of electric servomotor **120**, activating it and controlling the displacement of actuator piston **122**.

Actuator piston **122** pushes directly on skirt **101b** of primary piston **101**, thereby pushing primary piston **101**.

In general, during normal operation, the brake system of FIG. 1 is actuated by a force exercised on brake pedal PF, which displaces control rod **155** and plunger piston **150**. The displacement of the plunger piston or the control rod is detected by sensor **160**, which informs control circuit **200**. This circuit actuates servomotor **120** for the braking action. Actuator piston **122** is displaced in direction A to push primary piston **101**, which first delivers the fluid in brake circuit C then compresses the hydraulic fluid in primary chamber **102** and supplies hydraulic fluid under pressure to wheel brakes circuit C. This operation is the same whether the master cylinder is a simple master cylinder or a tandem master cylinder with a primary piston, a secondary piston, a primary chamber, and a secondary chamber.

During this normal braking activity, thrust rod **141** is not in contact with plunger cylinder **150**, an interval between these two elements being controlled by control circuit **200** through the actuating movement of primary piston **101**. During this movement, the reaction on the pedal is provided by the reaction engendered by return spring **152**.

Operation of the brake system of FIGS. 1, 1A will be described in detail together with the operation of the second embodiment shown in FIGS. 2, 2A, followed by the exceptional operating conditions of this brake system.

FIGS. 2 and 2A illustrate a second embodiment of the vehicle brake system with an electric servomotor and hydraulic reaction piston and drag compensation according to the invention, which differs from the first embodiment in that reaction spring **130** of hydraulic reaction piston **140** consists of a principal spring, **130a**, and an auxiliary spring, **130b**; the other elements that are identical to the first embodiment have the same reference numbers and their description will not be repeated.

Principal spring **130a** is housed between retaining organ **133**, integral with skirt **101b**, near the exterior extremity of the skirt, and a floating support, **145**, in the shape of a washer, which slides in skirt **101b** and makes contact with shoulder **101h**, limiting the displacement of floating support **145** in the direction of release of principal spring **130a** (direction A).

Auxiliary spring **130b** is installed between the back of floating support **145** and stop **142** of hydraulic reaction piston **140**. Stop **142** is, in this example, equipped with a spacer ring, **143**, intended to press against the back of floating support **145** to limit the compression and compaction of auxiliary spring **130b** and directly transmit the thrust of reaction piston **140** to floating support **145**.

Distance S, which separates the edge of ring **143** from the back of floating support **145**, is the distance that reaction piston **140** can travel in compressing auxiliary spring **130b**. Distance S represents the relative movement between primary piston **101** and reaction piston **140** at the start of a braking action enabling drag compensation.

Principal spring **130a** and auxiliary spring **130b**, constituting reaction spring **130**, are combined in series, that is, they act upon one another. The hardness of auxiliary spring **130b** is relatively low and its preloading is, for example, on the order of 30 N, whereas the hardness of principal spring **130a** is

significant. This means that if a force is exerted in direction B on hydraulic reaction piston **140**, primary piston **101** being considered fixed, reaction piston **140** first compresses auxiliary spring **130b** until peripheral ring **143** rests against the back of floating support **145**. At that moment, auxiliary spring **130b** no longer plays a role and the force is directly transmitted by stop **142** and peripheral ring **143** of reaction piston **140** to floating support **145** in such a way that, from this moment, principal spring **130a** will be compressed.

Please note that, as in FIG. 1, in FIG. 2 the extremity of thrust rod **141** of hydraulic reaction piston **140** is not in contact with the forward face of plunger piston **150** when the brake system is at rest or operating normally, and no exceptional braking is taking place.

FIG. 3 is a diagram illustrating the different operating curves of a servomotor brake system.

These diagrams represent, along the abscissa, the force applied to control rod **155** through brake pedal PF. This force is represented in N units. The ordinate represents the pressure occurring in primary chamber **102** of master cylinder **100**, whether it is a simple master cylinder or a tandem master cylinder. This pressure is indicated in bars.

All the curves shown have in common an initial phase, PH1 during which the force applied to control rod **155** does not result in any increased pressure in master cylinder **100**. This initial phase corresponds to the compensation of play in the kinematic chain of the brake system.

At the end of this first phase, there is, under appropriate conditions, a PH2 jump, corresponding to the sudden transition from zero pressure (with respect to the outside pressure) in master cylinder **100** to a higher, even relatively high pressure.

Three cases are envisaged:

The first case (curve C1) is that of the absence of a mechanism creating a jump in the servobrake. For example, this is represented by an embodiment such as that shown in FIG. 1. Servobrake **120** begins to act directly, based on the null pressure in the master cylinder. The pressure then increases, the right segment corresponding to the rise in pressure provided by the servobrake. The action of the servobrake is, for example, limited to a pressure of 100 bars.

The second curve, C2, shown with a solid line, corresponds to a known servobrake. The jump pressure is relatively low, on the order of 15 to 20 bars. At the end of jump phase PH2, the pressure in the master cylinder will increase due to the action of the servomotor (phase PH3). At the end of the intervention of the servomotor (for example, at a pressure of 100 bars), the force component can be supplied only by forceful action on the brake pedal. Segment PH4, extending the right segment corresponding to phase PH3 of the intervention of the servomotor, is a steeper straight line, D4, combining two actions—that of the servomotor, which is then limited to its maximum intervention, and the progressive, forceful action exerted by the driver on brake pedal PF.

Curve C3, a dashed line, represents the operation of the system of FIG. 2. The PH2 jump is significant and depends on the hardness of principal spring **130a**. After the jump period, PH2, there is a period of intervention by the servomotor, PH3, until a customary maximum pressure is reached in the master cylinder, which is generally 100 bars. This is followed by the combined action of the intervention of the servobrake and the forceful thrust exerted on the brake pedal (phase PH4).

In the absence of a forceful thrust, that is, under normal braking conditions, the action is limited to phase PH3, intervention by the servomotor.

Operation of brake system **2**, 2A will be described below in greater detail with the help of FIGS. 4 to 10, corresponding to this second embodiment; the operation of the first, simpler, embodiment can be deduced during the course of the explanation.

As shown by FIG. 4, starting from the initial rest position of the different elements of the combination, control circuit **200**, which detects an initial displacement of control rod **155**, actuates servomotor **120** so that actuator piston **122** compensates for the play in the kinematic and hydraulic chain by pushing primary piston **101**. This travel is relatively short. During this travel, plunger piston **150** remains pressed against rear wall **123** of body **121** of electric servomotor **120**.

This movement has no influence on pedal travel. A certain volume of brake fluid is displaced by the movement of the actuator piston under low pressure, for example, on the order of 2 to 3 bars, and, as shown, reduces mechanical play as well as hydraulic play by pre-filling the brake cylinders. This situation and position of the elements corresponds to the onset of drag compensation.

FIG. 5 shows the end of the drag compensation movement. Actuator piston **122** has repelled primary piston **102** by generating increased pressure in primary chamber **102**, which has displaced reaction piston **140**, exposed to the pressure in primary chamber **102**, with respect to primary piston **102**, in direction B. This movement compresses auxiliary spring **130b** until spacer ring **143** rests against the back of floating support **145**. Auxiliary spring **130b** is thereby compressed to the maximum allowed by threshold S. Floating support **145** is then applied against shoulder **144** in external chamber **101c**. During this phase, spring **130a** is not compressed. The driver begins to press on the pedal. Because of the servo action managed by control **2**, thrust rod **141** of reaction piston **140** is not in contact with the front of plunger piston **150**.

FIG. 6 illustrates the jump phase—the continuation of the action of servomotor **120**, controlled by maintaining pressure on brake pedal PF, and the displacement of control rod **155** with plunger piston **150**. This movement is detected by sensor **160**. Actuator piston **122** continues its movement of pressurizing primary chamber **102** by pushing directly on primary piston **101**. When pressure in primary chamber **102** is exerted on hydraulic reaction piston **140**, this compresses principal spring **130a** over a distance that depends on the stiffness of principal spring **130a**. Spring **130a** is chosen to provide the desired stiffness, that is, a given pressure level at the end of the jump (see FIG. 3).

As shown in FIG. 6, the travel of reaction piston **140** is relatively short during the jump with respect to primary piston **101**. There is no contact between thrust rod **141** and plunger piston **150**. Plunger piston **150** is subject to the reaction of return spring **152**, which creates the pedal sensation for the control rod and the foot pressing on the brake pedal, that is, the sensation of the reaction of the brake circuit.

According to FIG. 7, during this action of servobrake **120**, the driver exerts considerable force on pedal PF; this force is transmitted by the control rod **155** to plunger piston **150**, which compresses return spring **152** and touches the extremity of axial thrust rod **141** so that this force results in compression of the fluid in primary chamber **102** through the advance of hydraulic reaction piston **140**, actuator piston **122** maintaining the contact of primary piston **101**. During this phase, the driver perceives, through brake pedal PF, the force composed of the reaction of return spring **152**, augmented by

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the force of reaction piston **140** (its surface exposed to the pressure of primary chamber **102** multiplied by that pressure).

As shown in FIG. **8**, if the action on brake pedal PF is moderate, actuator piston **122** causes primary piston **101** to advance, producing a force on hydraulic reaction piston **140**, which compresses principal piston **130b** somewhat more. The differential travel, $\Delta 1$, between actuator piston **122** and plunger piston **150** is controlled and used for servo action by control circuit **200**. The force perceived by the driver at brake pedal PF and that of return spring **152** is augmented by the hydraulic force exerted on reaction piston **140** and decreased by the compressive force of principal spring **130a**, which compression is supplied by actuator piston **122**.

FIG. **9** shows the situation of the previous figure if the driver rapidly takes his foot off the brake pedal. Because reaction piston **140** is retained in primary piston **101** and the latter is retained by actuator piston **122**, there is no significant reaction that would be perceived by the driver. In effect, reaction piston **140** cannot withdraw (direction B) beyond the point where its shoulder **144** comes into contact with stop **101f** of primary piston **101**.

FIG. **10** illustrates emergency operation if electric servomotor **120** fails. Control rod **155** directly transmits the force of reaction piston **140** through plunger piston **150**, in direct contact with reaction piston **140**. Insertion of reaction piston **140** into primary chamber **102** creates sufficient pressure in the brake circuit for this emergency operation.

For these pressure levels, principal spring **130a** is not compressed by the differential movement between hydraulic reaction piston **140** and primary piston **101**.

Operation of the brake system according to the embodiment of FIGS. **1A**, **1B** corresponds in practice to that described above for the brake system of FIGS. **2**, **2A**; the initial phase shown in FIG. **4** also applies to the first embodiment. Only the operating phase shown in FIG. **5**, corresponding to drag compensation, does not exist. Subsequently, operation is the same as that shown in FIGS. **6** to **10**.

The present invention applies to the vehicle brake systems industry.

What is claimed is:

1. An electric-servomotor vehicle brake system, comprising:

a master cylinder including a primary piston delimiting therein a primary chamber connected by a brake fluid circuit to wheel brake cylinders;

an electric servomotor including an actuator piston acting on the primary piston;

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a control rod connected to a brake pedal and displacing a plunger piston to actuate the master cylinder, when applicable with an assistance of the electric servomotor; a sensor for detecting a movement of the control rod and for informing a control circuit of the electric servomotor, wherein:

the master cylinder, the servomotor, and the control rod are aligned on an axis, and

the primary piston delimits the primary chamber in the master cylinder and is formed from a body that, on an outside of the master cylinder, is extended by a cylindrical skirt forming an external chamber;

a reaction spring housed in the external chamber and including an end pressing against a retaining organ integral with the skirt, wherein:

the body includes an axial through hole connecting a rear wall of the external chamber and the primary chamber, and

the actuator piston cooperates directly with the skirt to push the primary piston; and

a hydraulic reaction piston housed in the axial through hole of the body of the primary piston and integrally bearing an axial thrust rod on an exterior, the hydraulic reaction piston including a stop against which another end of the reaction spring rests, wherein the stop rests against the rear wall of the external chamber to one of push the primary piston and be pushed by the primary piston.

2. The vehicle brake system according to claim **1**, wherein: the reaction spring includes a principal spring and an auxiliary spring combined in series and separated from one another by a floating support that is movable with respect to a stop of the primary piston to limit an expansion stroke of the principal spring, and

the auxiliary spring is of a reduced hardness with respect to the principal spring so the auxiliary spring can be compressed before the principal spring.

3. The vehicle brake system according to claim **2**, wherein the stop of the hydraulic reaction piston includes a ring that cooperates with the floating support in compressing the auxiliary spring to limit a compression of the auxiliary spring and thereby rest directly against the floating support.

4. The vehicle brake system according to claim **1**, wherein the retainer organ is a disc traversed by the thrust rod.

5. The vehicle brake system according to claim **1**, wherein the thrust rod includes a shoulder that cooperates with the retainer organ to determine an extreme end-of-travel position for the hydraulic reaction piston.

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